

# EE2013

## NON-LINEAR CIRCUIT ANALYSIS

### LECTURE 19: OPAMP POSITIVE FEEDBACK

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Coordinator: Prof. Pádraig Cantillon-Murphy

# LECTURE SCHEDULE

Thursdays 11am-1pm  
(with short break)

Monday 9am-10am slot not used!

# LECTURE NOTES

<https://www.jaeger.ie/ee2013/lec17>

Uploaded before lecture takes place

## QUESTIONS?

Just ask whenever it comes to you!

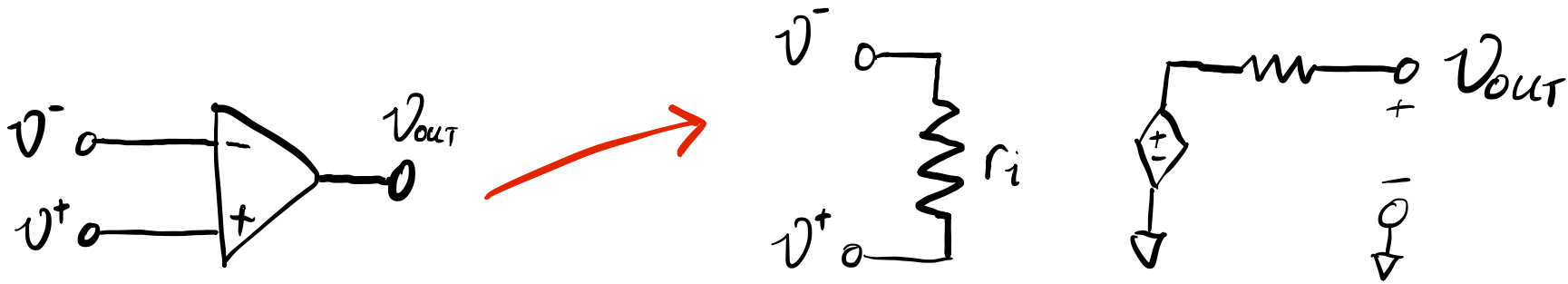
OR:

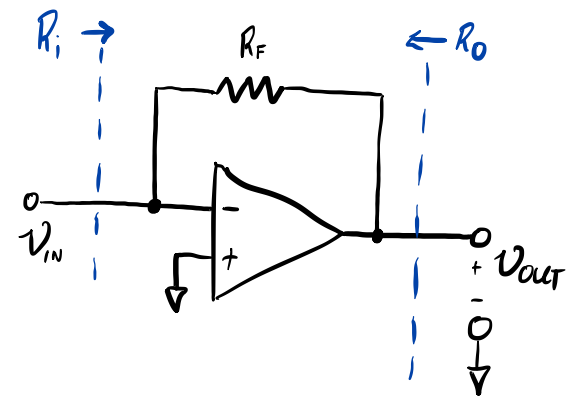
[anthony.wall@mcci.ie](mailto:anthony.wall@mcci.ie) on Email, Teams or Canvas

# 1 Review from Last Time

## 1.1 Op Amp Input and Output Resistance

To analyse the input and output circuit resistance in op amp circuits, we need to add a test source and improve the model of the op amp by adding internal input ( $r_i$ ) and output ( $r_o$ ) resistances.





This improved model allows us to calculate the input and output resistance given here for the inverting op amp amplifier:

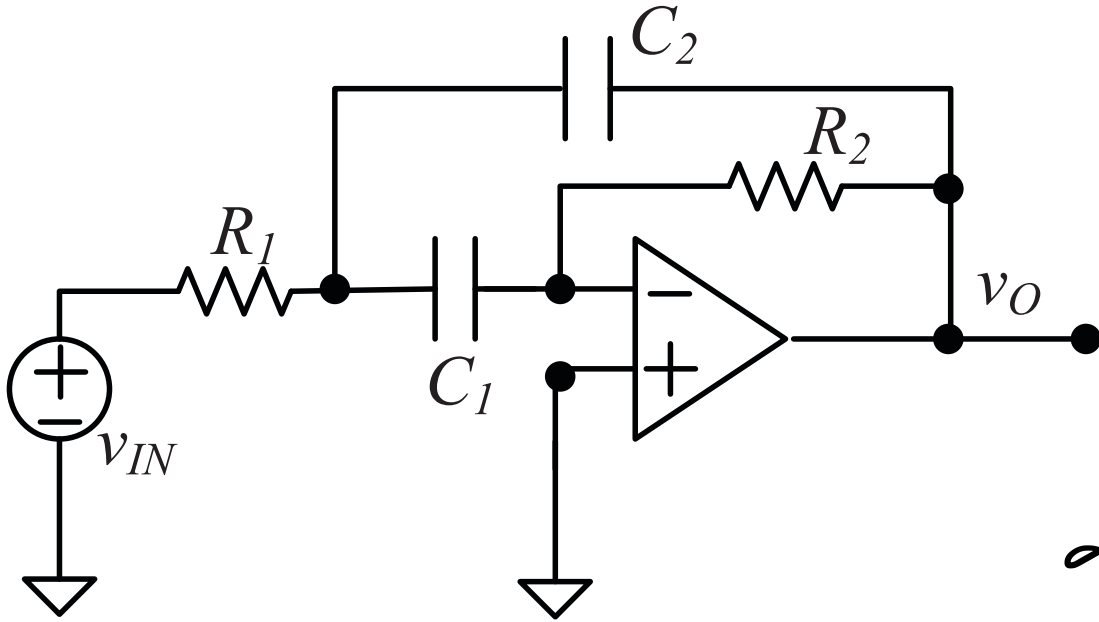
$$R_i = R_S + \frac{R_F + r_o}{A} \approx R_S \quad \leftarrow \text{Dominant}$$

The input resistance should be dominated by the series input resistance.

$$R_o = \frac{r_o}{1 + A \frac{R_S}{R_S + R_F}} \approx \frac{r_o(R_S + R_F)}{AR_S} \quad A \gg 1$$

### 1.2 Active Op Amp Filters

Active op amp filter circuits, like the bandpass filter below, eliminate the need for planar inductors in high-current VLSI circuits.



$$s^2 + 2\alpha s + \omega_0^2 = 0$$

*Active Bandpass:*

$$\omega_0 = \sqrt{\frac{G_1 G_2}{C_1 C_2}}$$

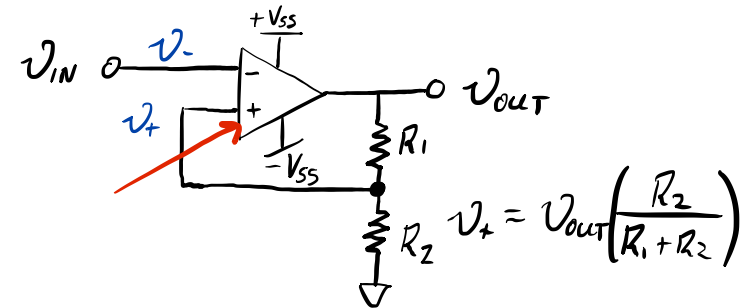
$$\alpha = \frac{(C_1 + C_2) G_2}{2 C_1 C_2}$$

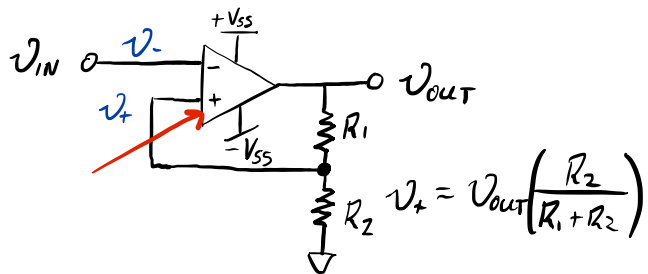
$$v_{OUT} = A(v_+ - v_-)$$

## 2 Positive Feedback and Op Amps

To date, we have only considered op amp circuits with negative feedback. However, what happens to the non-inverting amplifier circuit if we switch the input terminals to create positive feedback?

In this configuration, the op amp is **bistable** because once  $v^+ - v^-$  becomes slightly positive (negative) the op amp immediately saturates to  $+V_S$  ( $-V_S$ ) due to the large positive gain,  $A$ . The op amp remains at  $+V_S$  ( $-V_S$ ) until  $v^+ - v^-$  becomes negative (positive).





In the circuit shown,  $v^- = v_{IN}$  so the condition for positive saturation assuming that the op amp is initially negatively saturated becomes:

$$A(v^+ - v^-) = A\left(-\frac{V_S R_2}{R_1 + R_2} - v_{IN}\right) > 0$$

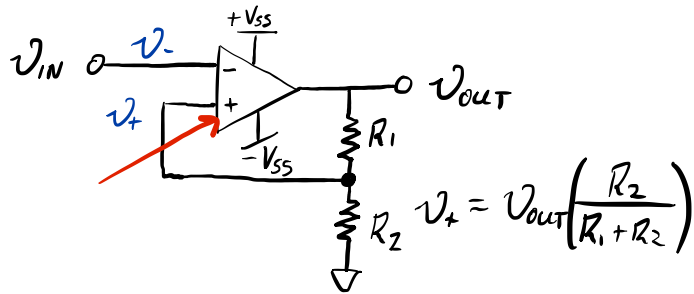
$v_{OUT} = -V_S$   $V_{SS} = V_S$   $-V_{SS} = -V_S$

For  $R_1 = R_2 = R$ :

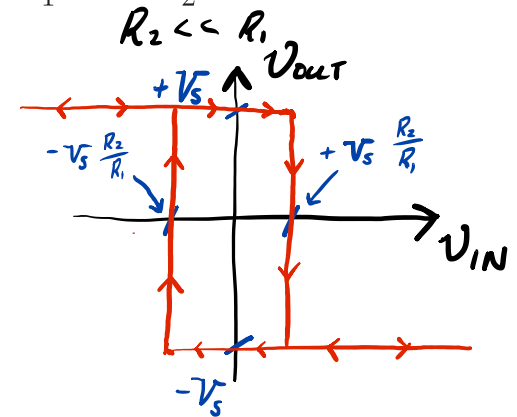
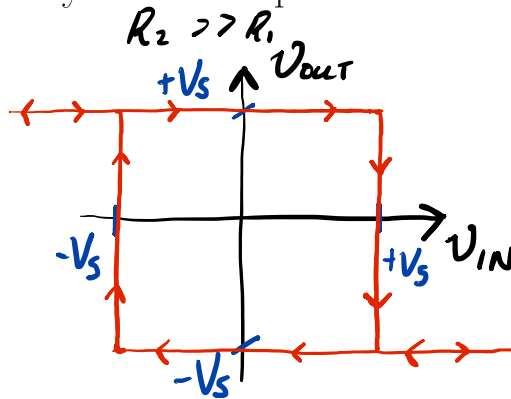
$$A\left(-\frac{V_S}{2} - v_{IN}\right) > 0$$

Since  $A$  is positive,  $v_{IN} < -\frac{V_S}{2}$  changes the output from negative ( $-V_S$ ) to positive ( $+V_S$ ) saturation. The output remains in this state until  $v_{IN} > \frac{V_S}{2}$ , at which point, the output again reverts to  $-V_S$ .





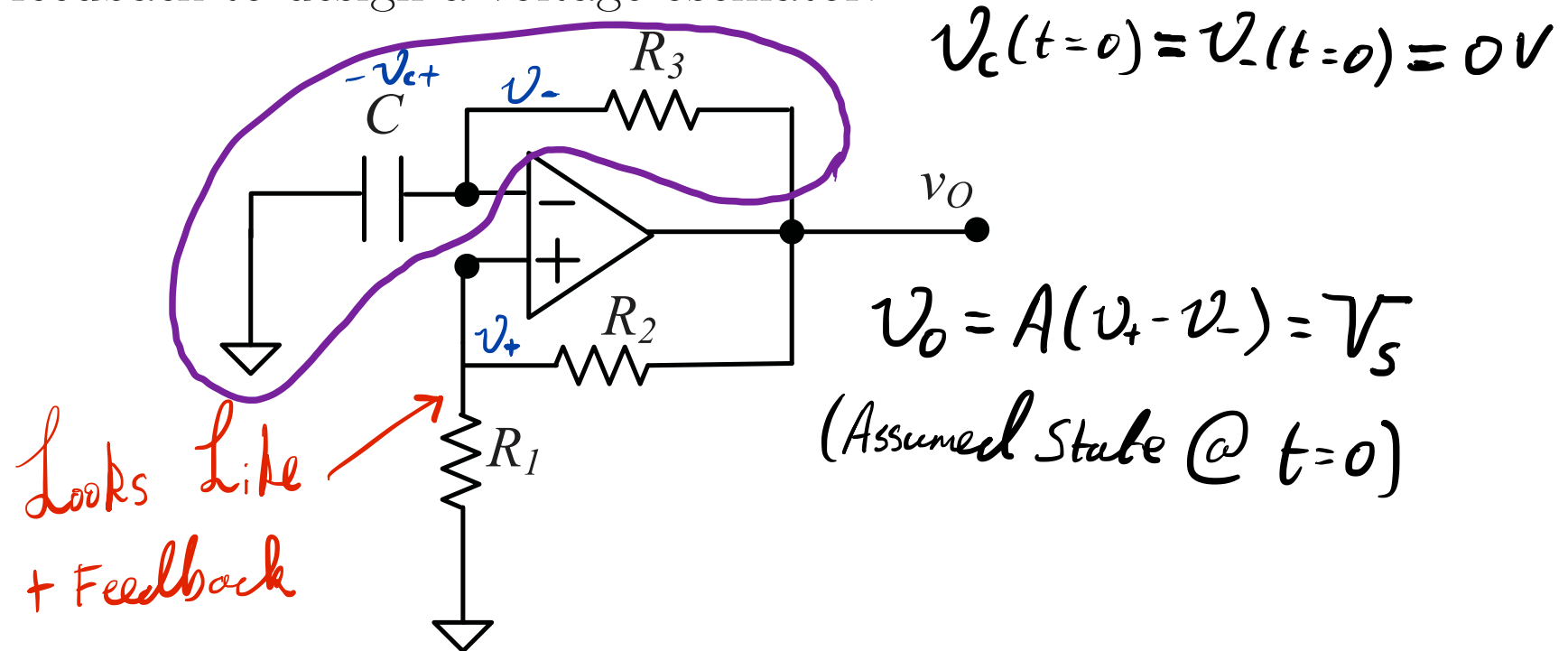
The phenomenon by which the output depends on the past input as well as the present input is known as *hysteresis*. Hysteresis results in the loop in the  $v_{IN} - v_O$  relation where the width of the hysteresis loop is controlled by  $R_1$  and  $R_2$ .





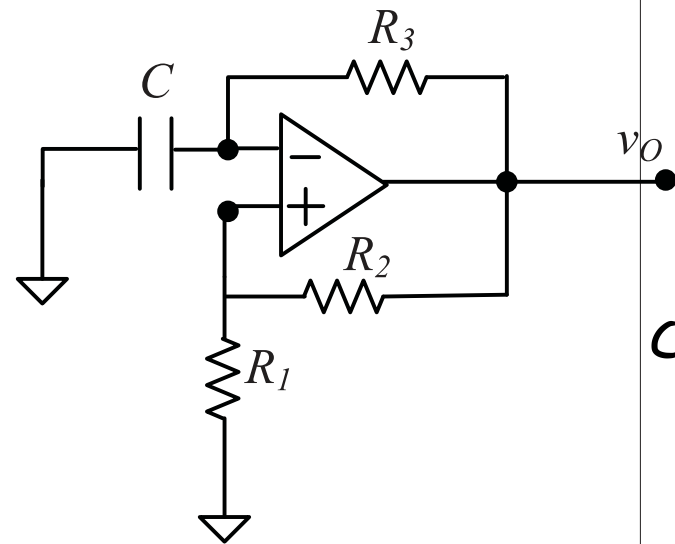
### 3 The Op Amp Voltage Oscillator

Positive feedback results in op amp saturation, which is useful in some situations. By including  $RC$  elements, we can use positive feedback to design a voltage oscillator.

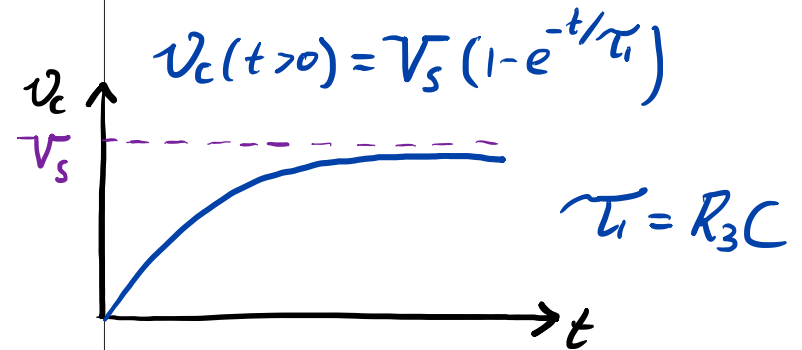
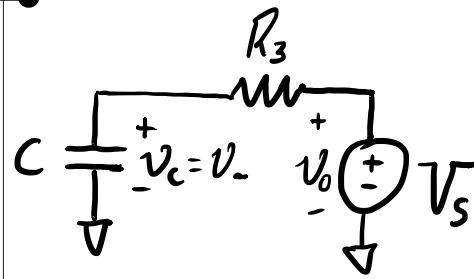


With the capacitor initially in the uncharged state ( $v_C = v^- = 0$ ), the output is positive:  $v_o = A(v^+ - v^-) = V_s$ .

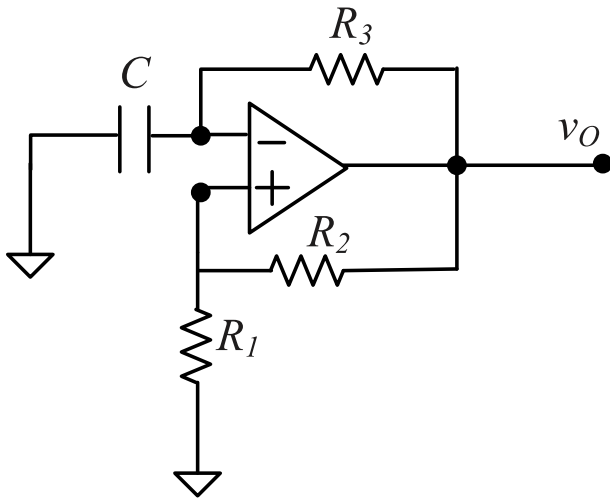
$$v_+ = v_o \frac{R_1}{R_1 + R_2} = V_s \frac{R_1}{R_1 + R_2}$$



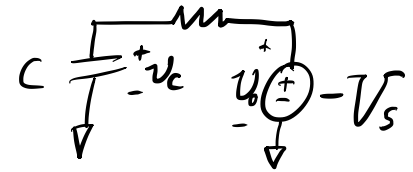
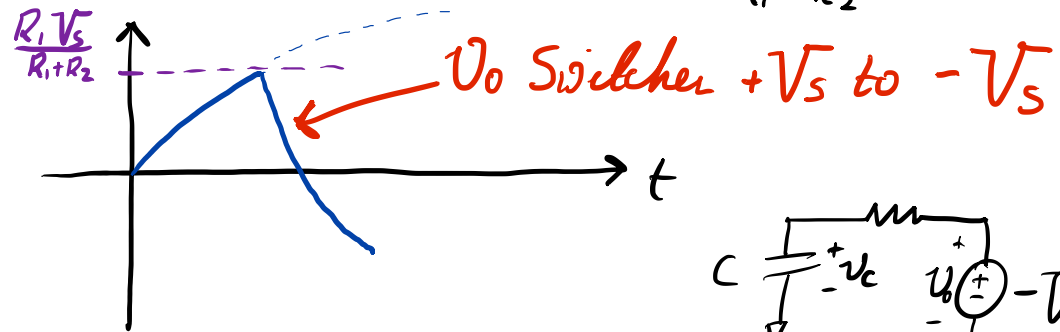
However, since the  $v^-$  terminal represents a large input impedance, the output voltage causes the capacitor to begin charging.



As the capacitor charges,  $v_C = v^-$  will eventually exceed  $v^+ = \frac{R_1 V_S}{R_1 + R_2}$  resulting in the output,  $v_O = A(v^+ - v^-)$ , switching from positive ( $+V_S$ ) to negative ( $-V_S$ ). This happens when:



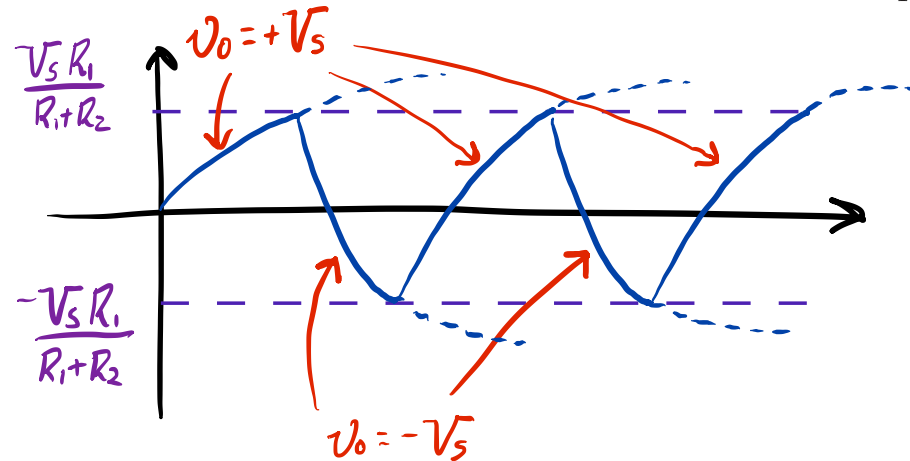
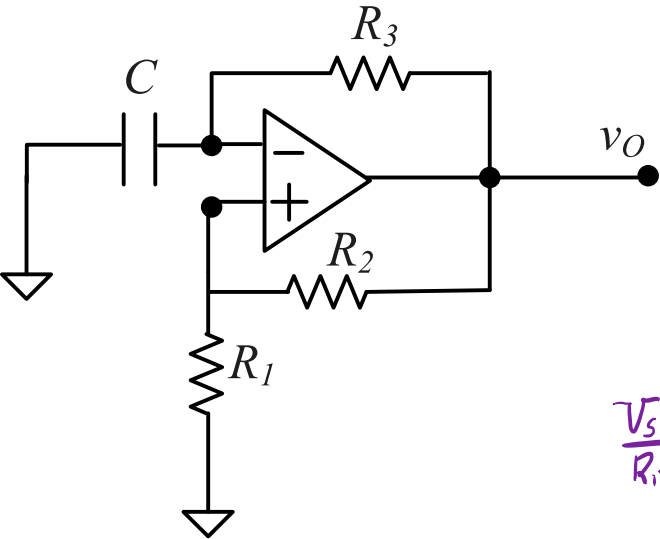
$$v_c = v^- > v^+ \\ V_S(1 - e^{-t/\tau}) > \frac{R_1 V_S}{R_1 + R_2}$$



Once the output changes to  $-V_S$ , the positive input,  $v^+$ , also changes:

$$v^+ = \frac{R_1 v_O}{R_1 + R_2} = -\frac{R_1 V_S}{R_1 + R_2}$$

Now, the partially charged capacitor has a higher voltage than the output voltage and begins to discharge through  $R_3$ . The capacitor continues to discharge until  $v_C = v^- = -\frac{V_S R_1}{R_1 + R_2}$



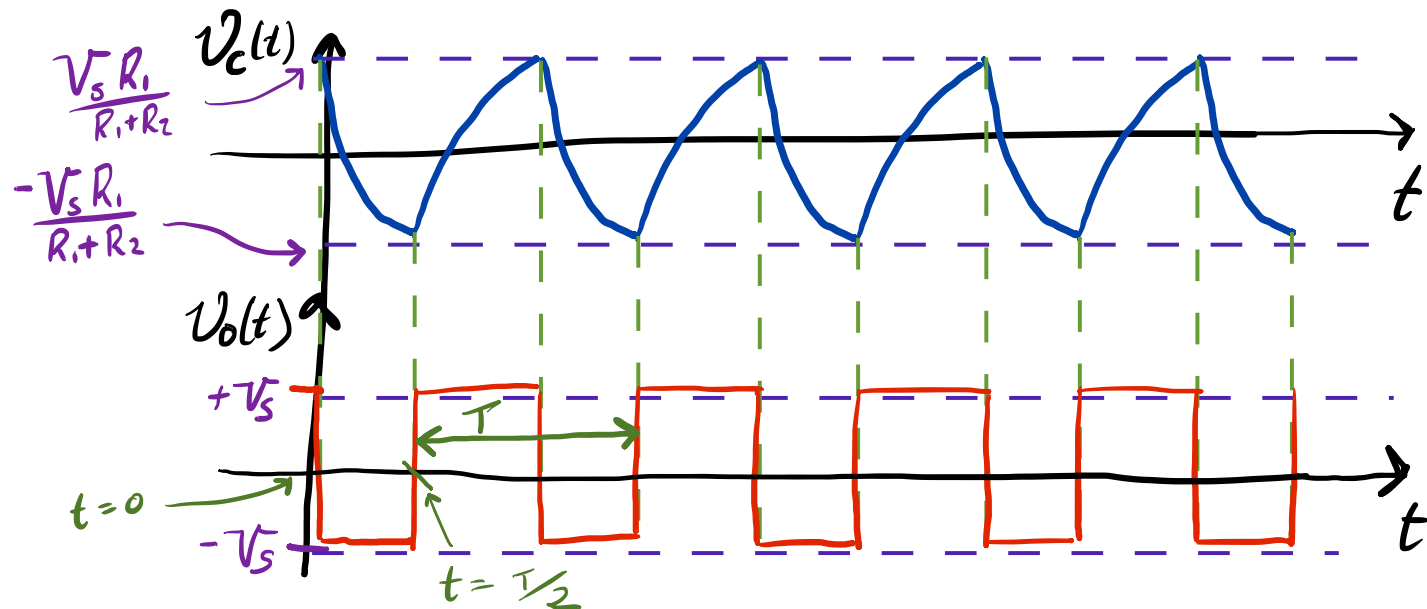
As soon as the capacitor voltage then exceeds  $-\frac{R_1 V_S}{R_1 + R_2}$ , this causes  $A(v^+ - v^-)$  to turn positive and the op amp returns to positive saturation:

$$v_o = +V_S$$

$$v_+ = \frac{R_1 V_S}{R_1 + R_2}$$

The capacitor then begins charging again and so on, the process repeating itself everytime that the capacitor voltage satisfies the condition:

$$v_c(t) = \pm \frac{V_S R_1}{R_1 + R_2}$$







### 3.1 Oscillator Time Constants

An important parameter is the oscillation period,  $T$ , which depends on the component values. To determine  $T$ , consider the discharging cycle of the capacitor:

$$v_C(t=0^-) = v_C(t=0^+) = \frac{V_S R_1}{R_1 + R_2}$$

Since  $v_O = -V_S$  at  $t = 0^-$ , the final possible capacitor voltage at  $v_C(t \gg \tau_1)$  is  $-V_S$ . In general:

$$\text{Initial} \xrightarrow{\quad} v_C(t) = \underbrace{v_C(0^+)}_{\text{Initial}} e^{-t/\tau} + \underbrace{v_C(t \gg \tau)}_{\text{Final Value} \rightarrow -V_S} (1 - e^{-t/\tau})$$

$$\Rightarrow v_C(0 < t < T/2) = \frac{V_S R_1}{R_1 + R_2} e^{-t/\tau} + (-V_S)(1 - e^{-t/\tau})$$

The output voltage switches from  $-V_S$  to  $+V_S$  at  $t = T/2$ , at which point:

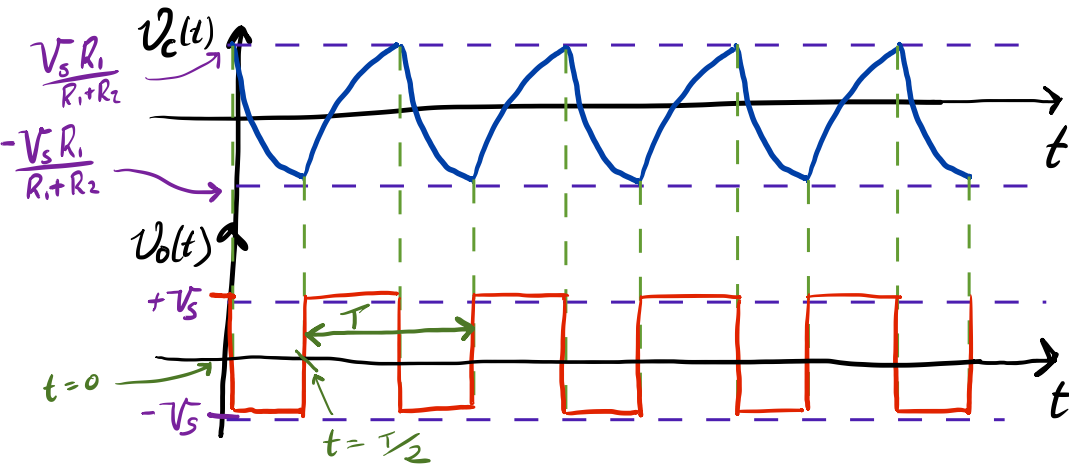
$$v_C(t = T/2) = \frac{R_1 V_S}{R_1 + R_2} e^{-T/(2\tau_1)} - V_S + V_S e^{-T/(2\tau_1)} = \frac{-V_S R_1}{R_1 + R_2}$$

$$e^{-T/(2\tau_1)} \left( \frac{R_1}{R_1 + R_2} + 1 \right) = 1 - \frac{R_1}{R_1 + R_2}$$

$$e^{-T/(2\tau_1)} \left( \frac{R_1 + R_2 + R_1}{R_1 + R_2} \right) = \frac{R_2}{R_1 + R_2}$$

$$e^{-T/(2\tau_1)} = \frac{R_2}{2R_1 + R_2}$$

$$-\frac{T}{2\tau_1} = \ln\left(\frac{R_2}{2R_1 + R_2}\right)$$

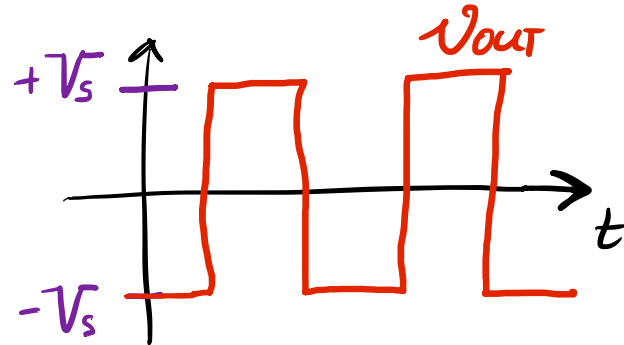
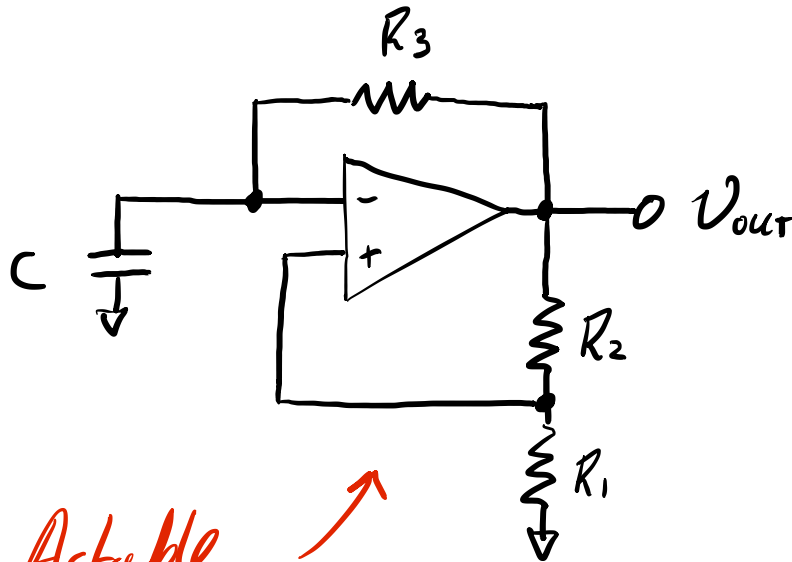


$$\frac{T}{2\tau_1} = \ln\left(\frac{2R_1 + R_2}{R_2}\right) = \ln\left(\frac{2R_1}{R_2} + 1\right)$$

$$T = 2\tau_1 \ln\left(\frac{2R_1}{R_2} + 1\right)$$

$$T = 2R_3C \ln\left(\frac{2R_1}{R_2} + 1\right)$$

This is the simplest op amp oscillator design and is the basis for the 555 timer IC.



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